IN THE SPECIFICATION:

Page 4, the paragraph beginning at line 5 has been amended as follows:

Figure 1 shows a schematic exemplary embodiment of a multi-beam recording element in a laser recording device. The multi-beam recording element essentially comprises a drive circuit 1, a laser beam generator 2, an optical lens 3 and an objective 4. The laser beam generator 2 is designed as a strip-shaped laser diode arrangement, called a laser diode bar in brief. The strip-shaped laser diode arrangement is composed of a plurality — five in the illustration — of laser diodes 5 arranged in a row and spaced from one another. The laser diodes 5, whose emitters can be individually driven with the drive circuit 1, are located on a common substrate carrier 6. The substrate ~~carrier6~~ carrier 6 is arranged such that the laser beams 7 generated by the laser diodes 5 emerge from the laser beam generator 2 parallel to an optical axis 8 of the multi-beam recording element.

Page 6, the paragraph beginning at line 10 has been amended as follows:

The disruptive thermal and optical crosstalk of the channels onto neighboring channels is compensated according to the invention by electronic feedback of correction signals K onto at least the immediately neighboring channels. The correction signals K for neighboring channels are acquired from the video signal V or from the driver current I_T of the channel lying between the neighboring channels. The acquisition of the correction signals K occurs with linear or non-linear ~~quadripoles~~ correction units whose transfer functions correspond to the time curves of the temperature T = f(t) or the light power P = f(t) in at least the immediately neighboring channels caused by the crosstalk.

Page 7, the paragraph beginning at line 12 has been amended as follows:

Subsequently, the time curve of the temperature $T_B = f(t)$ of the laser diode 5_B or of the light power $P_B = f(t)$ is simulated by an electrical ~~quadripole~~ correction unit and is input into a first correction unit 14. The ~~quadripole~~ correction unit can be designed as a linear low-pass that — in the simplest case — is constructed of an RC element, preferably of a combination of RC elements. The determination of "R" and "C" of the RC elements occurs by polynomial approximation according to known calculating methods. The required time curve of the driver current $I_B = f(t)$ is determined and employed for the scaling of the transfer function of the ~~quadripole~~ correction unit, being determined from the known relationship between the light power P and the driver current I_B, which is assumed to be approximately linear at least in the operating range, and from the measured function $P_B = f(t)$.